

- (ii) Conservation of linear momentum
- Remember Q is opposite direction so negative initially

$$m_1 u_1 + m_2 u_2 = m_1 v_1 + m_2 v_2$$

$$\therefore mu - kmu = mv + km \frac{u}{3}$$

$$\therefore v = u - ku - \frac{ku}{3} = u - \frac{4}{3}ku$$

$$\therefore v = \left(1 - \frac{4}{3}k\right)u.$$

- (iii) If motion of P is reversed after the collision, v will be in opposite direction and therefore negative.

$$\therefore 1 - \frac{4}{3}k < 0 \quad \text{so} \quad \frac{4}{3}k > 1 \quad \text{and} \quad k > \frac{3}{4}$$

- (iv) If coefficient of restitution in collision is 0.5

$$e = \frac{\text{Speed of separation}}{\text{Speed of approach}} = \frac{v_2 - v_1}{u_1 - u_2} \quad \begin{array}{ll} u_1 = u & v_1 = v \\ u_2 = -u & v_2 = \frac{1}{3}u \end{array}$$

$$\therefore \frac{1}{3}u - v = e(u - (-u))$$

$$\therefore \frac{1}{3}u - \left(1 - \frac{4}{3}k\right)u = \frac{1}{2} \cdot 2u$$

$$\therefore \frac{1}{3} - 1 + \frac{4}{3}k = 1$$

$$\therefore k = \frac{5}{3} \times \frac{3}{4} = \frac{5}{4}$$

If $k = \frac{5}{4}$ then $v = \left(1 - \frac{4}{3} \times \frac{5}{4}\right)u = -\frac{2}{3}u.$

$$\therefore v = -\frac{2}{3}u \quad \text{and} \quad k = \frac{5}{4}.$$

(b) $u = \begin{pmatrix} 3 \\ 2 \end{pmatrix}$ $u = \begin{pmatrix} 0 \\ 0 \end{pmatrix}$
 (A) (B)
 5 3

(i) $F = \begin{pmatrix} 1 \\ -2 \end{pmatrix}$ for 9 seconds on B using 'F=ma'
 $\begin{pmatrix} 1 \\ -2 \end{pmatrix} = 3 \begin{pmatrix} a_x \\ a_y \end{pmatrix}$ $\begin{pmatrix} a_x \\ a_y \end{pmatrix} = \begin{pmatrix} 1/3 \\ -2/3 \end{pmatrix}$

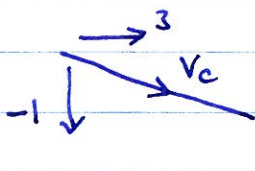
Using $v = u + at$ where $u = \begin{pmatrix} 0 \\ 0 \end{pmatrix}$, a from above, $t = 9$
 $\therefore v_B = \begin{pmatrix} 3 \\ -6 \end{pmatrix}$

Using CLM $m_A u_A + m_B u_B = m_C u_C$ [before = after]

$\therefore 5 \begin{pmatrix} 3 \\ 2 \end{pmatrix} + 3 \begin{pmatrix} 3 \\ -6 \end{pmatrix} = 8 \begin{pmatrix} v_x \\ v_y \end{pmatrix}$

$\therefore 8 \begin{pmatrix} v_x \\ v_y \end{pmatrix} = \begin{pmatrix} 24 \\ -8 \end{pmatrix}$

$\therefore v_C = \frac{1}{8} \begin{pmatrix} 24 \\ -8 \end{pmatrix} = \begin{pmatrix} 3 \\ -1 \end{pmatrix}$

(ii)  barrier is in direction $\begin{pmatrix} 0 \\ 1 \end{pmatrix}$ $\uparrow$ so vertical
 $e = \frac{1}{2}$

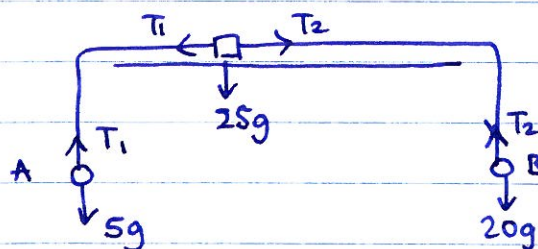
Only the perpendicular component is changed by the coefficient of restitution; the parallel component remains unaltered.

After impact

$\leftarrow -3e = -\frac{3}{2}$
 $\downarrow -1$

$\therefore v_{after} = \begin{pmatrix} -3/2 \\ -1 \end{pmatrix}$

2(a)



(i) Released from rest.

(A) Mechanical energy is preserved since table is smooth and no energy lost via friction so no work done; secondly gravity is not used on the block.

(B) No work is done by the block against reaction of table on it as table is smooth; motion is parallel to table surface.

(ii) $u=0$ $v=1.5 \text{ ms}^{-1}$ at Point P.

Work done = force $\times$ distance (in direction of motion)

change in p.e. = mgh

B moves down as largest mass $\therefore mgh = 20gh - 5gh = 15gh$

change in k.e. = $\frac{1}{2}m(v^2 - u^2)$

Total mass in the system = $20 + 5 + 25 = 50$

$$\therefore \text{k.e.} = \frac{1}{2} \times 50 \times (1.5^2 - 0^2)$$

$$\therefore 15gh = 25 \times 2.25$$

$$\therefore h = 0.383 \text{ metres.}$$

so OP is 0.383 metres.

(iii) Beyond P, table has friction. PQ is 2 metres in which 25g block does 180 J work against resistance to motion. Speed at Q is v .

change in k.e. = $\frac{1}{2}m(v^2 - u^2) = \frac{1}{2} \times 50 \times (v^2 - 1.5^2)$

work done between P + Q = mgh for system - Friction work done

$$\therefore \text{change in p.e.} = 20g \times 2 - 5g \times 2 - 180$$

$$\therefore 30g - 180 = 25(v^2 - 2.25)$$

$$\therefore v^2 = 6.81$$

$$\therefore v = 2.61 \text{ ms}^{-1}$$

$\therefore$ speed at Q is 2.61 ms^{-1}

(b) tree mass 450 kg slope 20° incline; steady speed = 2.5 ms^{-1}

$\therefore$ no acceleration. Frictional force = 2000 N

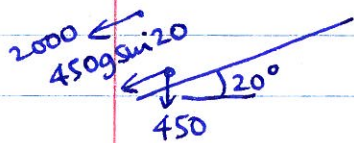
$$\text{Power} = Fv = \frac{fd}{t}$$

$$\text{Downward force} = 450g \sin 20^\circ + 2000$$

$$\therefore P = (450g \sin 20^\circ + 2000) \times 2.5$$

$$\therefore P = 8771 \text{ Watts}$$

$$\therefore \text{Power} = 8770 \text{ Watts (3sf).}$$



Q3.
(i)



Take moments about R_A .

$$\text{CW } 85 \times 3$$

$$\text{ACW } R_B \times 5$$

$$\therefore 5 R_B = 3 \times 85$$

$$\therefore R_B = 51 \text{ N.}$$

Resolving vertically

$$R_B + R_A = 85$$

$$\therefore R_A = 85 - 51$$

$$\therefore R_A = 34 \text{ N.}$$

or Taking moments about R_B

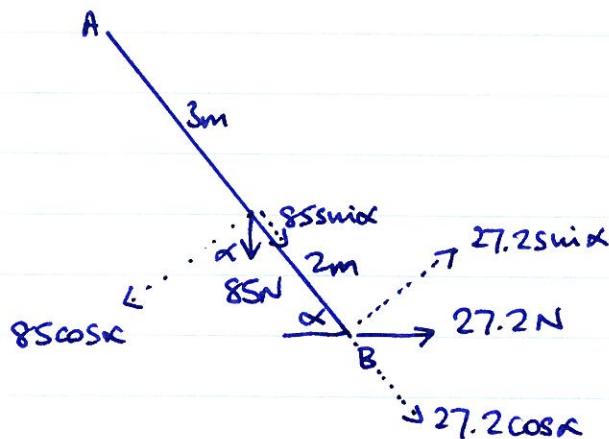
$$\text{CW: } R_A \times 5$$

$$\text{ACW } 85 \times 2$$

$$\therefore 5 R_A = 2 \times 85$$

$$\therefore R_A = 34 \text{ N.}$$

(ii)



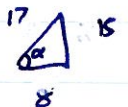
taking moments about A means we can ignore reaction force there. Resolving force at B and weight. Only forces perpendicular to beam produce moments about A.

$$\text{Moments about A: } \begin{array}{ll} \text{ACW} & 27.2 \sin \alpha \times 5 \\ \text{CW} & 85 \cos \alpha \times 3 \end{array}$$

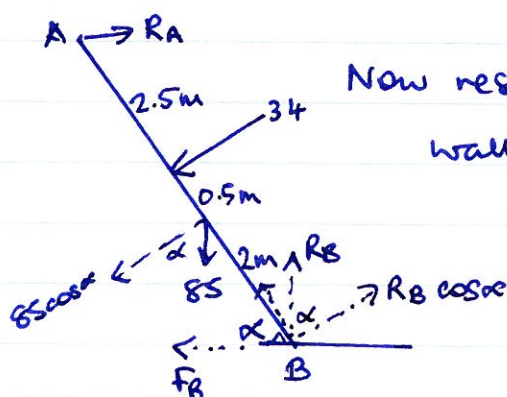
$$\therefore 27.2 \sin \alpha \times 5 = 85 \cos \alpha \times 3$$

$$\therefore \frac{\sin \alpha}{\cos \alpha} = \frac{85 \times 3}{27.2 \times 5}$$

$$\therefore \tan \alpha = \frac{15}{8} \quad \therefore \cos \alpha = \frac{8}{17} \text{ and } \sin \alpha = \frac{15}{17}$$



(iii)



Now resting on a rough floor and smooth wall - friction on the floor but not on the wall: on the point of slipping.

could resolve $R_B \sin \alpha$ and $R_B \cos \alpha$ as above



Better to take moments about A since we want to exclude those reaction forces

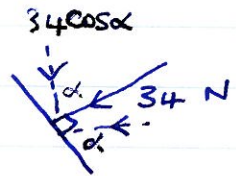
$$\text{CW} \quad 34 \times 2.5 + 85 \cos \alpha \times 3 + F_B \sin \alpha \times 5$$

$$\text{ACW} \quad R_B \cos \alpha \times 5$$

$$\therefore 205 + \frac{75}{17} F_B = \frac{40}{17} R_B$$

$$\cos \alpha = \frac{8}{17}$$

$$\sin \alpha = \frac{15}{17}$$



Resolving vertically

$$34 \cos \alpha + 85 = R_B$$

$$\therefore R_B = 101 \text{ N.}$$

$$\therefore F_B = 7.4 \text{ N}$$

Resolving horizontally

$$R_A = 34 \sin \alpha + F_B$$

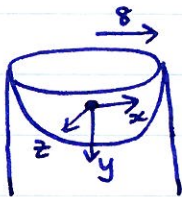
$$\therefore R_A = 37.4 \text{ N}$$

Given $F = \mu R$ for limiting friction

$$\mu = \frac{F}{R} = \frac{7.4}{101} = 0.073267...$$

$$\therefore \mu = 0.0733 \quad (3 \text{ sf}).$$

4.
(i)



part	mass (area)	x	y	z
bowl	$2\pi r^2 = 2\pi 64$	0	4	0
legs	$2\pi r \cdot h = \frac{16k\pi}{2\pi 64 + 16k\pi}$	0	$\frac{k}{2}$	0

$$M \begin{pmatrix} \bar{x} \\ \bar{y} \\ \bar{z} \end{pmatrix} = \sum m_i \begin{pmatrix} x_i \\ y_i \\ z_i \end{pmatrix}$$

$$\therefore (2\pi 64 + 16k\pi) \bar{y} = 2\pi 64 \times 4 + 16k\pi \times \frac{k}{2}$$

$$(64 + 8k) \bar{y} = 256 + 4k^2 \quad \div 2\pi$$

$$(16 + 2k) \bar{y} = 64 + k^2 \quad \div 4$$

$$\therefore \bar{y} = \frac{64 + k^2}{16 + 2k}$$

(ii) If $k=12$, plus a circular end underneath the bowl previously $\bar{y} = \frac{64+k^2}{16+2k}$ so when $k=12$, $\bar{y}=5.2$

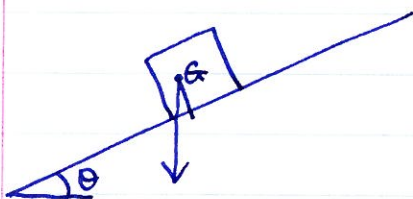
now	part	mass	y
	previous	320π	5.2
	end	64π	12

$$\therefore M \bar{y}_{\text{new}} = 320\pi \times 5.2 + 64\pi \times 12$$

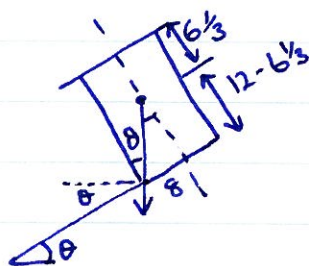
$$\therefore 384\pi \bar{y}_{\text{new}} = 1664\pi + 768\pi$$

$$\therefore \bar{y}_{\text{new}} = \frac{1664+768}{384} = 6\frac{1}{3} \text{ down from O.}$$

(iii)



Not sliding and on point of toppling.
Centre of mass directly over edge of toppling



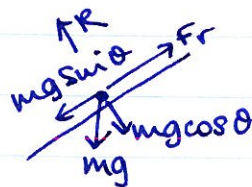
$$\tan \theta = \frac{8}{(12-6\frac{1}{3})} = \frac{8}{(5\frac{2}{3})} = \frac{24}{17}$$

$$\therefore \theta = \tan^{-1}\left(\frac{24}{17}\right) = 54.6887\dots$$

$$\therefore \theta = 54.7^\circ \quad (3sf)$$

(iv) If $\mu = 1.5$ will bowl still slide?

$$\mu = \frac{F}{R} \quad F \leq \mu R$$



$$R = mg \cos \theta \quad F = 1.5 \times mg \cos \theta$$

$$mg \sin \theta - Fr = mg \sin \theta - 1.5 mg \cos \theta = -0.05100\dots$$

so $mg \sin \theta - Fr < 0$ implies will not slide.

$$\text{or } \mu = \frac{F}{R} = \frac{mg \sin \theta}{mg \cos \theta} = \tan \theta = \frac{24}{17} = 1.41176\dots$$

Since given $\mu = 1.5 > 1.41\dots$ then will not slide.